Solutions to workshop 03: Rate law and stoichiometry

Lecture notes for chemical reaction engineering

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Try following problems from Fogler 5e(Fogler 2016).

P3-5, P3-10, P3-11, P3-12, P 4-6, P 4-8, P 4-11

We will go through some of these problems in the workshop.

P 3.12

Write the rate law for the following reactions assuming each reaction follows an elementary rate law. Give the units of k_A for each, keeping in mind some are homogeneous and some reactants are heterogeneous.

- 1. $C_2H_6 \longrightarrow C_2H_4H_2$
- 2. $C_2H_4 + \frac{1}{2}O_2 \longrightarrow C_2H_4O$
- 3. $(CH_3)_3COOC(CH_3)_3 \rightleftharpoons C_2H_6 + 2 CH_3COCH_3$
- 4. $nC_4H_{10} \Longrightarrow iC_4H_{10}$
- 5. $CH_3COOC_2H_5 + C_4H_9OH \Longrightarrow CH_3COOC_4H_9 + C_2H_5OH$
- 6. $2 \text{ CH}_3 \text{NH}_2 \rightleftharpoons (\text{CH}_3)_2 \text{NH} + \text{NH}_3$
- 7. $(CH_3CO)_2O + H_2O \Longrightarrow 2 CH_3COOH$

💡 Solution

$$\begin{split} &1. \ -r_A = kC_A \\ &2. \ -r_A = kC_A C_B^{1/2} \\ &3. \ -r_A = k\left(C_A - \frac{C_B C_C}{K}\right) \\ &4. \ -r_A = k\left(C_A - \frac{C_B}{K}\right) \\ &5. \ -r_A = k\left(C_A C_B - \frac{C_C C_D}{K}\right) \end{split}$$

$$\begin{aligned} \mathbf{6.} \ -r_A' &= k \left(P_A^2 - \frac{P_B P_C}{K} \right) \\ \mathbf{7.} \ -r_A &= k \left(C_A C_B - \frac{C_C^2}{K} \right) \end{aligned}$$

P3-10

The initial reaction rate for the elementary reaction $2 A + B \longrightarrow 4 C$ was measured as a function of temperature when the concentration of A was 2 M and that of B was 1.5 M.

$-r_A(mol/dm^3s)$	T(K)
0.002	300
0.046	320
0.72	340
8.33	360

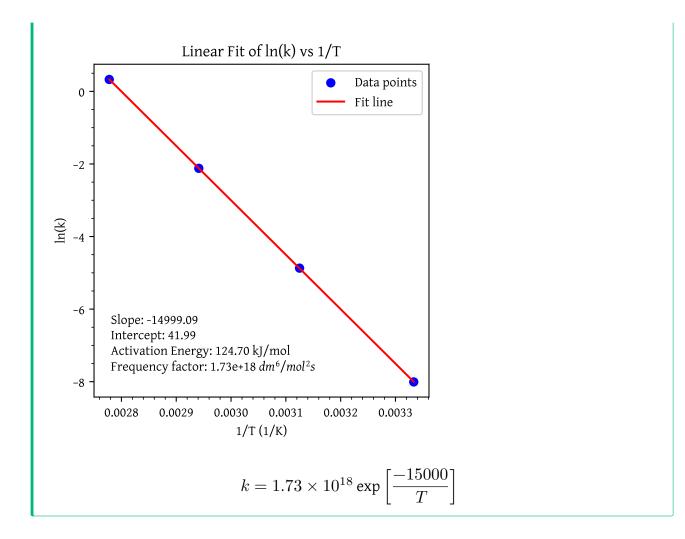
- 1. What is the activation energy?
- 2. What is the frequency factor?
- 3. What is the rate constant as a function of temperature using Equation 1 and T_0 = 27 °C as the base case?

$$k(T) = k(T_0)exp\left[\frac{E}{R}\left(\frac{1}{T_0} - \frac{1}{T}\right)\right] \tag{1}$$

Solution

 $\begin{array}{l} 2\,\mathrm{A} + \mathrm{B} \longrightarrow 4\,\mathrm{C}. \mbox{ Elementary reaction. Initial rates given.} \\ \mbox{For elementary reaction} \\ -r_A = k C_A^2 C_B \\ k = \frac{-r_A}{C_A^2 C_B} \\ \mbox{At the start of reaction:} \\ k = \frac{-r_{A0}}{C_{A0}^2 C_{B0}} \end{array}$

```
import numpy as np
import matplotlib.pyplot as plt
from scipy.stats import linregress
# Data
r_A = np.array([0.002, 0.046, 0.72, 8.33])
T = np.array([300, 320, 340, 360])
R = 8.314 \ \# \ J/mol \ K
C_A0 = 2.0
C B0 = 1.5
k = r_A/(C_A0**2 * C_B0)
ln_k = np.log(k)
inv_T = 1 / T
slope, intercept, r_value, p_value, std_err = linregress(inv_T, ln_k)
line = slope * inv_T + intercept
activation_energy = -slope*R/1000 # (kJ/mol)
A0 = np.exp(intercept)
# Plot
plt.scatter(inv_T, ln_k, color='blue', label='Data points')
plt.plot(inv T, line, color='red', label='Fit line')
# Labels and title
plt.xlabel('1/T (1/K)')
plt.ylabel('ln(k)')
plt.title('Linear Fit of ln(k) vs 1/T')
plt.legend()
slope_text = f'Slope: {slope:.2f}'
intercept_text = f'Intercept: {intercept:.2f}'
e_text = f'Activation Energy: {activation_energy:.2f} kJ/mol'
a0_text = f'Frequency factor: {A0:.2e} $dm^6/mol^2 s$'
plt.annotate(f'{slope text}\n{intercept text}\n{e text}\n{a0 text}', xy=(0.05, 0.25),
# Show plot
plt.show()
```



P 4-8

The gas-phase reaction

$$\frac{1}{2}\,N_2 + \frac{3}{2}\,H_2 \longrightarrow NH_3$$

is to be carried out isothermally first in a flow reactor. The molar feed is 50% H₂ and 50% N₂, at a pressure of 16.4 atm and at a temperature of 227 °*C*?.

- (a) Construct a complete stoichiometric table.
- (b) Express the concentrations in mol/dm^3 of each for the reacting species as a function of conversion. Evaluate C_{A0} , δ and ϵ , and then calculate the concentrations of ammonia and hydrogen when the conversion of H_2 is 60%.
- (c) Suppose by chance the reaction is elementary with $k_{N_2} = 40 \ dm^3/mol/s$. Write the rate of reaction solely as a function of conversion for
 - (1) a flow reactor, and for
 - (2) a constant-volume batch reactor.

Solution

Gas phase reaction

$$\frac{1}{2}\,N_2+\frac{3}{2}\,H_2\longrightarrow NH_3$$

 $\begin{array}{l} y_A = 0.5 \\ y_B = 0.5 \\ P = 16.4 atm \\ T = 227^\circ C = 500 K \end{array}$

a. stoichiometric table

Basis of reaction: H_2

$$H_2 + \frac{1}{3}N_2 \longrightarrow \frac{2}{3}NH_3; \qquad A + \frac{1}{3}B \longrightarrow \frac{2}{3}C$$

Species	Entering	Change	Exiting
A	F_{A0}	$-F_{A0}X$	$F_A = F_{A0}(1 - X)$
В	$F_{B0} = \Theta_B F_{A0}$	$-F_{A0}X/3$	$F_A =$
			$F_{A0}(\Theta_B-X/3)$
С	0	$+(2/3)F_{A0}X$	$F_C = (2/3)F_{A0}X$

□_B = 1

b. Conc. in mol/dm^3 as f(X)

$$\begin{split} \delta &= c/a - b/a - 1 = 2/3 - 1/3 - 1 = -2/3 \\ \epsilon &= y_{A0} \delta = 0.5 \delta = -1/3 \\ C_{A0} &= 0.2 \end{split}$$

 $C_A = \frac{C_{A0}(1-X)}{(1+\epsilon X)} \cdots \text{Constant P}$ and T

$$\begin{split} C_A &= \frac{C_{A0}(1-X)}{(1+X/3)} \to X = 0.6 \to C_A = \frac{0.2(1-0.6)}{(1+0.6/3)} = 0.1 mol/dm^3 \\ C_C &= \frac{2}{3} \frac{C_{A0}(X)}{(1+\epsilon X)} \to X = 0.6 \to C_C = \frac{2}{3} \frac{0.2 \times 0.6}{(1+0.6/3)} = 0.1 mol/dm^3 \end{split}$$

c. $-r_A$ as f(X) , $k_{N_2}=40 dm^3/mols$

1. Flow reactor

$$\begin{split} -r_{N_2} &= k_{N_2} C_{N_2}^{1/2} C_{H_2}^{3/2} \\ -r_{N_2} &= 40 \left[\frac{C_{A0}(\Theta_B - X/3)}{(1 + \epsilon X)} \right]^{1/2} \left[\frac{C_{A0}(1 - X)}{(1 + \epsilon X)} \right]^{3/2} \\ -r_{N_2} &= 40 C_{A0}^2 \left[\frac{(1 - X)}{(1 - X/3)} \right]^{3/2} = 1.6 \left[\frac{(1 - X)}{(1 - X/3)} \right]^{3/2} \end{split}$$

2. For constant volume batch reactor

$$-r_{N_2} = k_{N_2} C_{N_2}^{1/2} C_{H_2}^{3/2}$$

$$-r_{N_2} = 40 C_{A0}^2 (1-X/3)^{1/2} (1-X)^{3/2} = 1.6 (1-X/3)^{1/2} (1-X)^{3/2}$$

P 4-11

Consider a cylindrical batch reactor that has one end fitted with a frictionless piston attached to a spring (See Figure 1). The reaction

$$A+B \longrightarrow 8\,C$$

with the rate law

 $-r_A = k_1 C_A^2 C_B$

is taking place in this type of reactor.

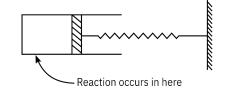


Figure 1: Cylindrical batch reactor

- (a) Write the rate law solely as a function of conversion, numerically evaluating all possible symbols.
- (b) What is the conversion and rate of reaction when $V = 0.2 ft^3$?

Additional information:

Equal moles of A and B are present at t_0

Initial volume: $0.15 ft^3$

Value of $k_1 : 1.0 \ (ft^3/lbmol)^2 \cdot s^{-1}$

The spring constant is such that the relationship between the volume of the reactor and pressure within the reactor is

V = (0.1) (P) (V in ft^3 , P in atm)

Temperature of system (considered constant): $140\ ^\circ F$

Gas constant: $0.73~ft^3atm/lbmol\cdot^\circ R$

💡 Solution

a. Rate law as f(X)

$$y_{A0} = \frac{N_{A0}}{N_{A0} + N_{B0}} = 0.5$$

$$\delta = 8 - 1 - 1 = 6$$

$$\epsilon = y_{A0}\delta = 3$$

$$V = V_0(1 + \epsilon X)\frac{P_0}{P}\frac{T}{T_0}$$

$$\begin{split} P_0 &= 10V_0; P = 10V \\ V &= \frac{10V_0^2}{10V}(1 + \epsilon X) \\ V^2 &= V_0^2(1 + \epsilon X) \\ N_A &= N_{A0}(1 - X); N_B = N_{A0}(\Theta_B - X) \\ \Theta_B &= \frac{N_{B0}}{N_{A0}} = 1 \\ -r_A &= kC_A^2C_B = \frac{kN_A^2N_B}{V^2} = \frac{kN_{A0}^3(1 - X)^3}{V_0^3(1 + \epsilon X)^3/2} \\ \frac{N_{A0}}{V_0} &= \frac{y_{A0}P}{RT} \\ \dot{n} - r_A &= k\left(\frac{y_{A0}P_0}{RT}\right)^3 \left(\frac{(1 - X)}{(1 + \epsilon X)^{1/2}}\right)^3 \\ -r_A &= 5.02 \times 10^{-9} \left(\frac{(1 - X)}{(1 + \epsilon X)^{1/2}}\right)^3 \\ b. \ X \ \text{and} \ -r_A \ \text{at} \ V &= 0.2 f t^3 \\ V^2 &= V_0^2(1 + \epsilon X) \\ (0.2)^2 &= (0.15)^2(1 + 3X) \Rightarrow X = 0.259 \\ -r_A &= 8.623 \times 10^{-10} lbmol/ft^3s \end{split}$$

Fogler, H. Scott. 2016. *Elements of Chemical Reaction Engineering*. Fifth edition. Boston: Prentice Hall.